

Weber-Fechner law in CIE 230:2019 for threshold colour differences of surface colours

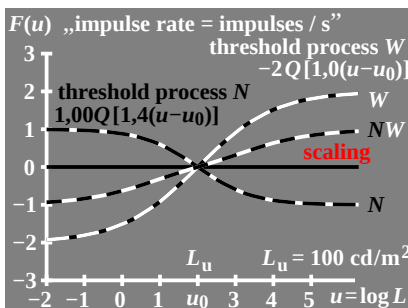
The Weber-Fechner law describes the lightness L^* as **logarithmic** function of L_u .
The Stevens law describes the lightness L^* as **potential** function of $L_u = Y/5$.
IEC 61966-2-1 uses a similar potential function $L_{TIC} = m L_u^{1/2.4}$.
The Weber-Fechner law is equivalent to the linear equation: $\Delta L_u = c L_u$ [1]
Integration leads to the logarithmic equation: $L^* = k \log(L_u)$ [2]
Derivation for $\Delta L_u = 1$ leads to the linear equation: $L_u / \Delta L_u = k_0 = 57$ [3]
For colours in offices the **standard contrast range** is 25:1=90:3.6

Table 1: CIE tristimulus value Y , luminance L , and lightness L^*

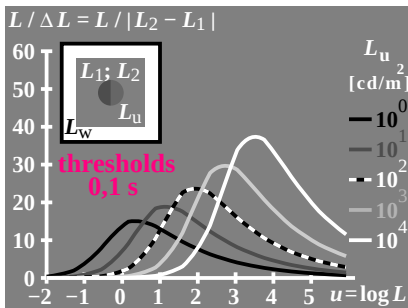
Colour (matte)	Tristimulus value Y	office luminance L [cd/m ²]	relative luminance $L_u = L/L_u$	CIE lightness L^* [Jz]	relative lightness $L^*_{rel} = L^*/L^*_{u=100}$
White W (paper)	90	142	5	94	44
Grey Z (paper)	18	28,2	1	50	0
Black N (paper)	3,6	5,6	0,2	18	-40

For the lightness range between $L^*_r = -40$ and 40 the constant is: $k = 40 \log(5) = 57$

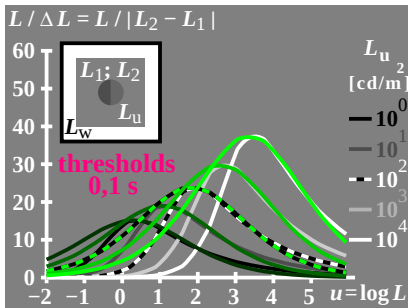
EE540-1N



EE540-3N



EE540-5N



EE540-7N

Weber-Fechner law in CIE 230:2019 for threshold colour differences of surface colours and two ranges $0.2 < L_u < 1$ and $1 < L_u < 5$

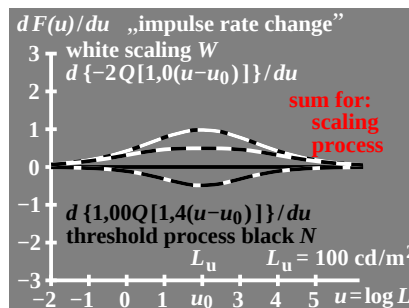
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IEC 61966-2-1 uses a similar potential function $L_{TIC} = m L_u^{1/2.4}$.
The Weber-Fechner law is equivalent to the linear equation: $\Delta L_u = c L_u$ ($c=0.1$) [1]
Integration leads to the logarithmic equation: $L^* = k_0 \log(L_u)$ ($c=0.1$) [2]
Derivation for $\Delta L_u = 1$ leads to the linear equation: $L_u / \Delta L_u = k_0 = 46$ ($k_0=46$, $k_1=63$) [3]
For colours in offices the **standard contrast range** is 25:1=90:3.6

Table 1: CIE tristimulus value Y , luminance L , and lightness L^*

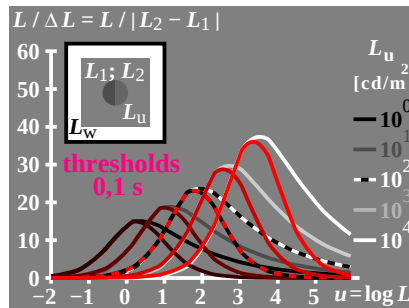
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White W (paper)	90	142	5	94	44
Grey Z (paper)	18	28,2	1	50	0
Black N (paper)	3,6	5,6	0,2	18	-32

For the two lightness ranges it is $k_0 = -32 \log(0.2) = 46$ and $k_1 = 44 \log(5) = 63$.

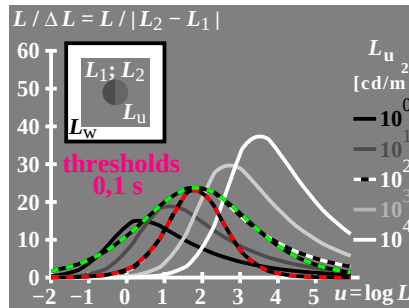
EE540-2N



EE540-4N



EE540-6N



EE540-8N

line element of Stiles (1946) with „color values” L_P, M_D, S_T

three separate color signal functions

$$F(L_P) = i \ln(1 + 9 L_P)$$

$$F(M_D) = j \ln(1 + 9 M_D)$$

$$F(S_T) = k \ln(1 + 9 S_T)$$

Taylor-derivations:

$$\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$$

$$= \frac{9i}{1+9L_P} \Delta L_P + \frac{9j}{1+9M_D} \Delta M_D + \frac{9k}{1+9S_T} \Delta S_T$$

EE541-1N

functions $q[k(u-u_0)]$ „achromatic signal”-description

with $u = \log L$ (L = luminance)
 $u_0 = \log L_u$ (L_u = surround luminance)

$$q[k(u-u_0)] = 1 + 1/[1 + \sqrt{2} e^{k(u-u_0)}]$$

function values:

$$q[k(u-u_0) \rightarrow +\infty] = 1$$

$$q[k(u-u_0) = 0] = \sqrt{2}$$

$$q[k(u-u_0) \rightarrow -\infty] = 2$$

EE541-3N

„achromatic signal” discrimination as function of relative light density $h = \ln H = k(u-u_0)$, $\ln$ = natural log.

$$Q' = \frac{d}{dH} [\ln \{1 + 1/(1 + \sqrt{2} H)\}] / \ln \sqrt{2}$$

$$= -\sqrt{2} / [\ln \sqrt{2} (1 + \sqrt{2} H)(2 + \sqrt{2} H)]$$

function values:

$$Q'[k(u-u_0) \rightarrow +\infty] = 0$$

$$Q'[k(u-u_0) = 0] = -0,5$$

$$Q'[k(u-u_0) \rightarrow -\infty] = 0$$

EE541-5N

double line element of Richter (1987) for the lighting technology with the luminance $L = f(L_P, M_D, S_T)$

$$F(L) = \int_{-\infty}^L (L/\Delta L) dL \text{ (relative lightness?)}$$

$$F(L) = iQ(H) = \begin{cases} iQ(H) & (u < u_0) \\ iQ(\bar{H}) & (u \geq u_0) \end{cases}$$

with: $k=1,4$ $\bar{k}=1$ $i=1$ $\bar{i}=-2$
 $u = \log L$ $u_0 = \log L_u$
 $H = e^{k(u-u_0)}$ $\bar{H} = e^{\bar{k}(u-u_0)}$ $\bar{H} = e^{\bar{k}(u-u_0)}$

EE541-7N

line element of Vos&Walraven (1972) with „color values” L_P, M_D, S_T

three separate color signal functions

$$F(L_P) = -2i\sqrt{L_P}$$

$$F(M_D) = -2j\sqrt{M_D}$$

$$F(S_T) = -2k\sqrt{S_T}$$

Taylor-derivations:

$$\Delta F(L_P, M_D, S_T) = \frac{dF}{dL_P} \Delta L_P + \frac{dF}{dM_D} \Delta M_D + \frac{dF}{dS_T} \Delta S_T$$

$$\Delta F(L_P, M_D, S_T) = \frac{i}{\sqrt{L_P}} \Delta L_P + \frac{j}{\sqrt{M_D}} \Delta M_D + \frac{k}{\sqrt{S_T}} \Delta S_T$$

EE541-2N

„achromatic signal”-description functions $Q_{1m}[k(u-u_0)]$

with $u = \log L$ (L = luminance)
 $u_0 = \log L_u$ (L_u = surround luminance)

$$Q_{1m}[k(u-u_0)] = \frac{1}{\ln \sqrt{2}} \ln q[k(u-u_0)] - m$$

function values with $l = m = 1$:

$$Q[k(u-u_0) \rightarrow +\infty] = 1$$

$$Q[k(u-u_0) = 0] = 0$$

$$Q[k(u-u_0) \rightarrow -\infty] = -1$$

EE541-4N

luminance discrimination possibility $L/\Delta L$ as function of H

with: $L = 10^u$ $H = e^h = 10^{\log e k(u-u_0)}$
 $dL/du = \ln 10 L$ $dH/du = k H$

it follows: $L/\Delta L = [kH / (dH \ln 10)]$
 $\frac{L}{\Delta L} = \text{const } H / [(1 + \sqrt{2} H)(2 + \sqrt{2} H)]$

$$Q'[k(u-u_0) \rightarrow +\infty] = 0$$

$$Q'[k(u-u_0) = 0] = \text{maximum}$$

$$Q'[k(u-u_0) \rightarrow -\infty] = 0$$

EE541-6N

double line element of Richter (1987) for the lighting technology with the luminance $L = f(L_P, M_D, S_T)$

$$F(L) = \int_{-\infty}^L (L/\Delta L) dL \text{ (relative lightness?)}$$

$$F(L) = iQ(H) \quad H = e^{k(u-u_0)}$$

$$Q(H) = [\ln \{1 + 1/(1 + \sqrt{2} H)\}] / \ln \sqrt{2} - 1$$

Taylor-derivations:

$$\Delta F(L) = \frac{dF}{dL} \Delta L = i \frac{dQ}{dH} \Delta H$$

$$= -i\sqrt{2} \Delta H / [\ln \sqrt{2} (1 + \sqrt{2} H)(2 + \sqrt{2} H)]$$

EE541-8N

TUB-test chart EE54; Achromatic thresholds, contrast ($L/\Delta L$), and lightness L^*
Line element, contrast, and lightness according to Weber-Fechner, Stiles, and Vos&Walraven